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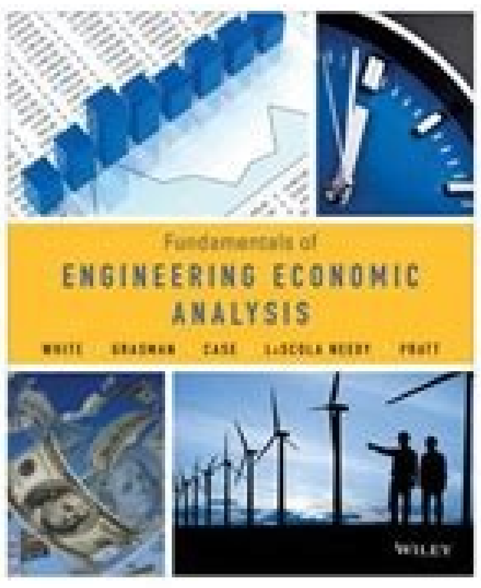
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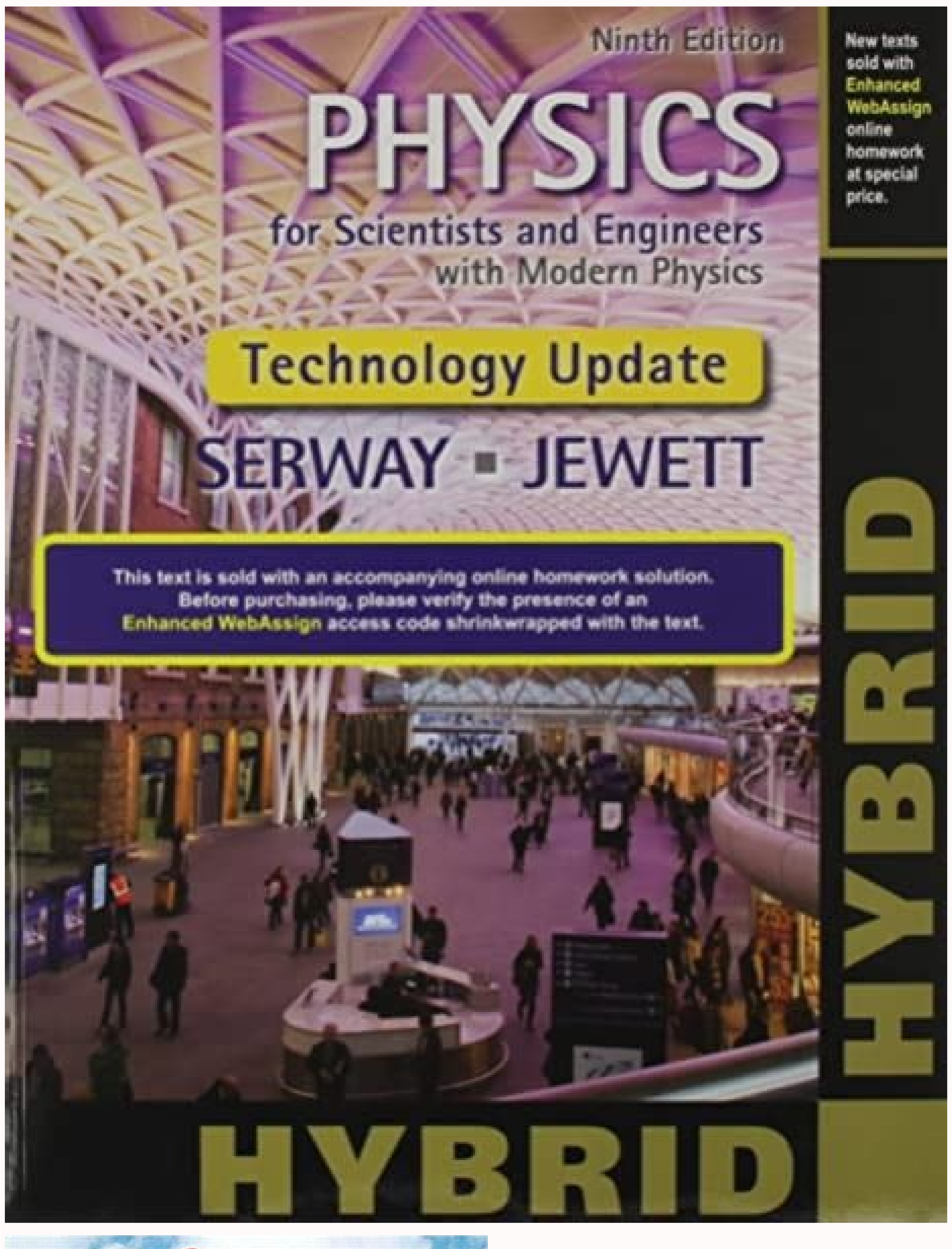
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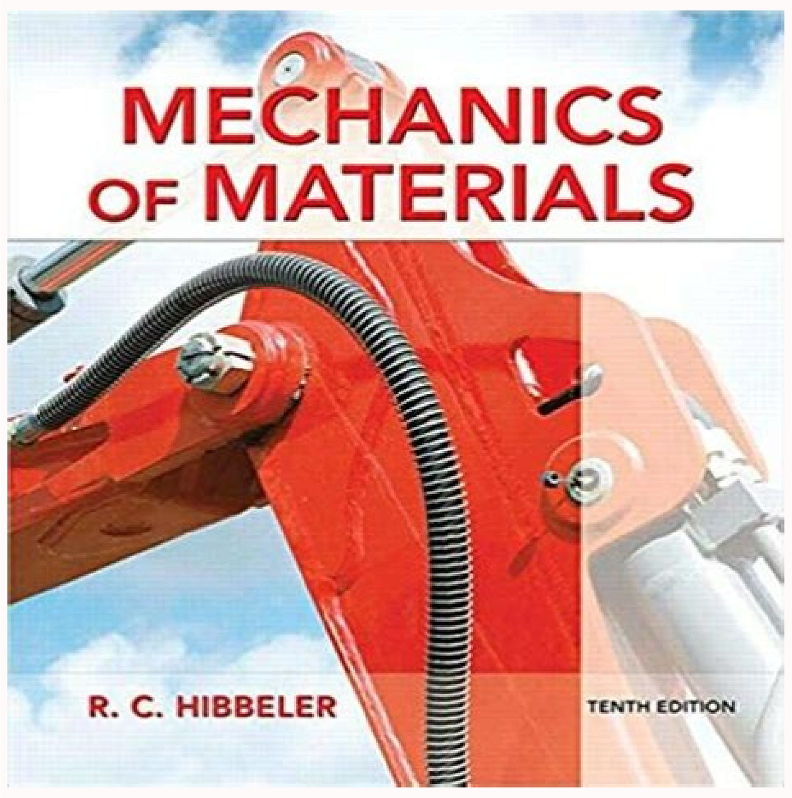
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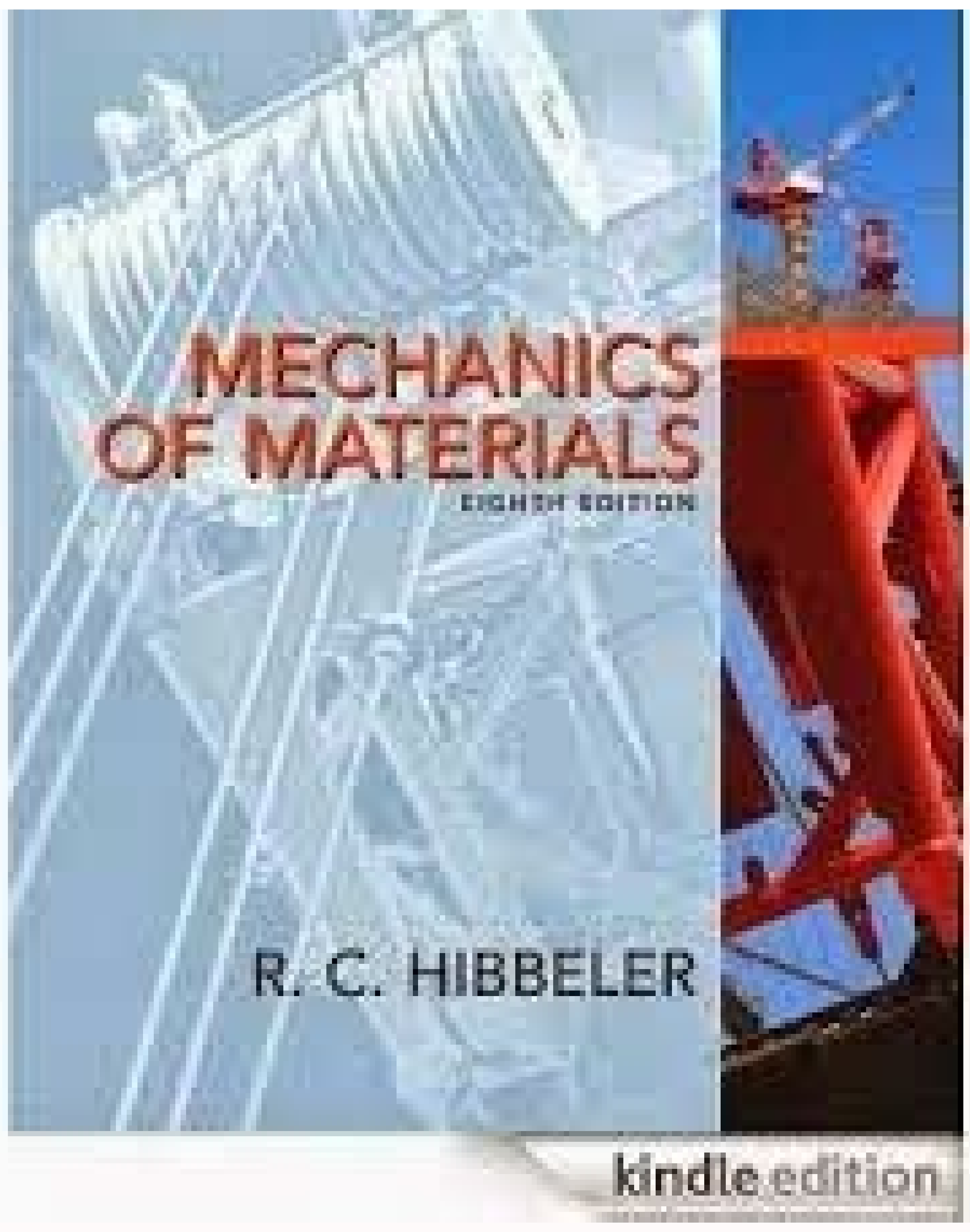

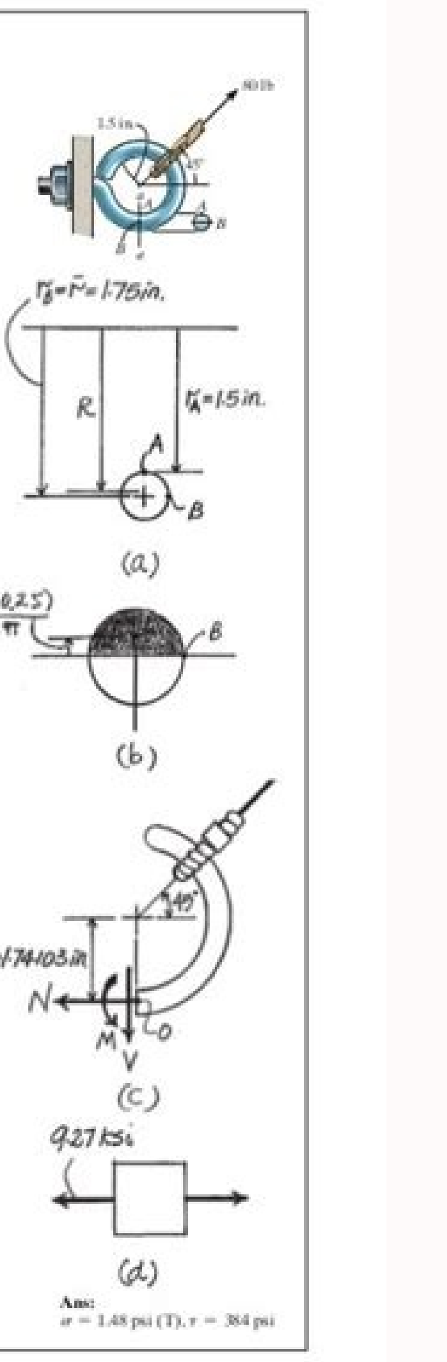

8–73.

The hook is subjected to the force of 80 lb. Determine the state of stress at point B at section a–a. The cross section has a diameter of 0.5 in. Use the curved-beam formula to calculate the bending stress.

SOLUTION

The location of the neutral surface from the center of curvature of the hook, Fig. a, can be determined from

$$R = \frac{A}{\Sigma \int_A \frac{dA}{r}}$$

where $A = \pi(0.25^2) = 0.0625\pi \text{ in}^2$

$$\Sigma \int_A \frac{dA}{r} = 2\pi\left(\bar{r} - \sqrt{\bar{r}^2 - c^2}\right) = 2\pi\left(1.75 - \sqrt{1.75^2 - 0.25^2}\right) = 0.11278 \text{ in.}$$

Thus,

$$R = \frac{0.0625\pi}{0.11278} = 1.74103 \text{ in}$$

Then

$$e = \bar{r} - R = 1.75 - 1.74103 = 0.0089746 \text{ in}$$

Referring to Fig. b, I and Q_B are computed as

$$I = \frac{\pi}{4}(0.25^4) = 0.9765625(10^{-3})\pi \text{ in}^4$$

$$Q_B = \bar{y}'A' = \frac{4(0.25)}{3\pi}\left[\frac{\pi}{2}(0.25^2)\right] = 0.0104167 \text{ in}^3$$

Consider the equilibrium of the FBD of the hook's cut segment, Fig. c.

$\xrightarrow{+} \Sigma F_x = 0;\quad N - 80\cos 45° = 0 \quad N = 56.57 \text{ lb}$

$+\uparrow \Sigma F_y = 0;\quad 80\sin 45° - V = 0 \quad V = 56.57 \text{ lb}$

$\circlearrowleft + \Sigma M_o = 0;\quad M - 80\cos 45°(1.74103) = 0 \quad M = 98.49 \text{ lb}\cdot\text{in}$

The normal stress developed is the combination of axial and bending stress. Thus,

$$\sigma = \frac{N}{A} + \frac{M(R - r)}{Aer}$$

Here, $M = 98.49$ lb · in since it tends to reduce the curvature of the hook. For point B, $r = 1.75$ in. Then

$$\sigma = \frac{56.57}{0.0625\pi} + \frac{(98.49)(1.74103 - 1.75)}{0.0625\pi(0.0089746)(1.75)}$$

$$= 1.48 \text{ psi (T)} \qquad \textbf{Ans.}$$

The shear stress is contributed by the transverse shear stress only. Thus,

$$\tau = \frac{VQ_B}{It} = \frac{56.57(0.0104167)}{0.9765625(10^{-3})\pi(0.5)} = 384 \text{ psi} \qquad \textbf{Ans.}$$

The state of stress of point B can be represented by the element shown in Fig. d.

Ans:
$\sigma = 1.48$ psi (T), $\tau = 384$ psi

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leets 0414 fo eceip lacirdnilyc a rof elbissop retemaid mumixam Eht animreted ot deksa ew 0,4 Now, you will repet this procedure for the mÃ¿Momandian ect ect = 4.12 gpa = Em Eph [1 çt' VFT]Ef + vft em (2.4 gpa) [131 gpa'] (1 Ã˜t] (131 gpa. 2.4 gpa) Solving this expression for vft for vFT = 0,4 ATE COME, DED I vfl and vft are iguales, the composed of it is possible. 15.17 The stypula problem that the transversal of a complex, ac, is of 320 mm2 (0.50 in.2), and the supply cargo, FC, is from 44.500 N
(10,000 lbff) for the compound of the 15.11.11.0 . (a) Primely, you're going to wet that we'll let's the Rapporteur FF/FM. Segean equation (15.11) EF VF (131 gpa)(0.30) FF = = = = 23.4 FM EME 2.4)(0.4) or, FF = . From FF + FM = FC = 44.500 N 23.4fm + FM = 44.500 N 56 P1: Fu/ft pb017-15 pb017-Callister September 18, 200 12:1 FF = 44.500 N A'' 1824 N = 42.676 N (9590 LBF) C) calculate the stem in each of the phases, is the first concory of the transversaries so of flus. This is determination as
AF = (0.30)(320 mm2) = 96 mm2 (0.15 in.2) Am = (0.70)(320 mm2) = 224 mm2 (0.35 in.2) Now, for tensions, f = FF 42676 N = 445 mpa (63.930 psis) = Af (96 mm2) m = FM 1824 N = 8.14 mpa (1170 : 224 mm2) The same cepa in each of each of the ones of marriage and fibra, as I2m = mp 8.14 mpa = 3.39 Ã— 10â^'3 in 2.4 Ã— = EF 131 Ã— 103 mpa 15.21 in this problem, to a compound of fibra fibra fiber gentle gentle glorifying, we are going to know that we will be the fibrdnal of the fiber (010 10 ,
The Middle Garden Longitud (2.5 mm), the volume of fibras (0.40), the force of fibre (3500 mpa), the UniÃ3n Fra-Marrix (75 mpa), the Uniã. .)aPM .)aPM 0.8(atseupmoc allaf ne zirtam al ed s©Ãrtse le onobrac le ,otnat ol roP .ominÃm le euq royam se n©Ãibmat euq)isp 002,292(aPM 5102 =)5.0( )aPM 0004(+)5.0( )aPM 03(= FV âË¢ÃF +)FVâ Ë¢Ã 1(M = âË¢ÃlC)71.51(n³Ãicauce al ed ,s¡AmedA .odacificepse ominÃm le euq royam se euq)isp 601 - £Ã 9.61(APG 6.611 =)5.0( )aPG 032(+)5.0( )aPG
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The general form of the equation used to calculate this relation is the equation (16.33) [or equation (16.32)] for the stag P-B ratio = ass2nd asn sno2 (150.69 g/mol) (7.30 g/cm3) = 1.33 (118.69 g/mol) (6.95 g/cm3) Therefore, the movie would probably be protective since this relationship is between one and two. 16.36 For this problem we are given weight gain data for the oxidation of Cu at a high temperature. a) We are asked first to determine if the oxidation kinetics obey a parab, linear or
logaride, expressions described by Equations (16.34), (16.35), and (16.36), respectively. One way to make this determination is by trial and error. Suppose the parabine relationship is vian; That is, of the equation (16.34) w2 = k1 t + k2 that means that we can establish three simultaneous equations using the three sets of values W and t given, then using two combinations of two pairs of equations, solve for K1 and K2 ; If K1 and K2 have the same values for both solutions, then the kinetics are parabólicos.
If the values are not identical then the other cynical relationships need to be explored. Asã, the three equations are (0.316) 2 = 0.100 = 15k1 + K2 (0.524) 2 = 0.275 = 50k1 + K2 (0.725) 2 = 0.526 = 100k1 + K2 60 P1: FNT PB017-16 PB017-Callister October 11, 2000 10:39 Char count = 0 of the first two equations k1 = 5 Ã— 10â^'3 and k2 = 0.025; These same two values are obtained using the last two equations. Therefore, the oxidation rate law is parabine. b) Since a parabic relationship is vian, this
part of the problem requires us W after a total time of 450 min. Again, using using1 x 10 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 x 1 = 1 x 1 = 1 x 1 = 1 x 1 = 1 x 1 = 1 x 1 = 1 x 1 = 1 = 1 x 1 = 1 x 1 = 1 = 1 x 1 = 1 = 1 x 1 = 1 = 1 x 2 = 1 = 1 x 1 = 1 = 1 = 1 = 1 x that is df − do = [1 + (tf − to)] now all we need to do is to establish expressions for df yields df = do [1 + (tf − to)] now all we need to do is to establish expressions for df (316 inox) and df (w), to establish them equal together, and to resolve
for tf. according to table 17.1, l (316 inox) = 16.0 × 10−6 in the form of C)−1 and l (w) = 4.5 × 10−6 (° C)−1 as well df (316 inox) = df (w) (9,988 mm)[1 + {16.0 × 10−6 (C) = 1 count(Tf - 25 °C)] = (10.000 mm) the phases is a pore phase, and that we estimate upper and lower limits for the room-temperature thermal conductivity of a magnesium oxide material having a 0.30 volume fraction of pores. The upper limit of k (kupper) may be determined using Equation (15.1) with thermal conductivity
substituted for the elastic modulus, E. From Table 17.1, the value of k for MgO is 37.7 W/m-K, while for still air in the pore phase, k = 0.02 W/m-K. Thus kupper = Vp kair + VMgO kMgO = (0.30)(0.02 W/m-K) + (0.70)(37.7 W/m-K) = 26.4 W/m-K For the lower limit we employ a modification of Equation (15.2) as klower = = kair kMgO Vp kMgO + VMgO kair (0.02 W/m-K)(37.7 W/m-K) = 0.067 W/m-K (0.30)(37.7 W/m-K) + (0.70)(0.02 W/m-K) 17.29 We want to heat the copper wire in order to reduce the
stress level from 70 MPa to 35 MPa; in doing so, we reduce the stress in the wire by 70 MPa ¢ÂÂÂ 35 MPa = 35 MPa, which will be a compressive stress (i.e., ¢ÃÂÂ35 MPa). Taking a value for E of 110 GPa (Table 7.1) and solving for Tf from Equation (17.8) Tf = To ¢ÂÂÂ E1 = 20¢ÂÂ¦Â C ¢ÂÂÂ ¢ÂÂÂ35 MPa (110 ÂÂ 103 MPa)(17 ÂÂ 10¢ÂÂÂ6 (¢ÂÂ¦Â C)¢ÂÂÂ1] = 20¢ÂÂ¦Â C + 19¢ÂÂ¦Â C = 39¢ÂÂ¦Â C (101¢ÂÂ¦Â F) 17.D1 This problem stipulates that 1025 steel railroad tracks are laid at a temperature of
10Ã°ÂC. We are asked to determine the hottest possible temperature that can be tolerated without the introduction of thermal stresses if the rails are 11.9 m long, and for a joint space of 4.6 mm. For these railroad tracks, each end is allowed to expand one-half of the joint space distance (4.6 mm). Equation (17.3a) is used to solve for Tf , where l for the 1025 steel is found in Table 17.1. Thus, Tf = To l = l + To l lo 4.6 ÂÂ 10¢ÂÂÂ3 m + 10¢ÂÂ¦Â C [12.0 ÂÂ
10¢ÂÂÂ6 (¢ÂÂ¦Â C)¢ÂÂÂ1] (11.9 m) = 32.2¢ÂÂ¦Â C + 10¢ÂÂ¦Â C = 42.2¢ÂÂ¦Â C (108¢ÂÂ¦Â F) 63 P1: FNT PB017-18 PB017-Callister September 18, 2000 15:20 Char Count= 0 CHAPTER 18 MAGNETIC PROPERTIES 18.1 This 752.1 or 1'â´â´â´â =1 =â˘â´â´â¸ m/H 6â´â´â´â ...

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